



Process development for deep drawing with integrated electromagnetic forming

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October 06, 2015*

- Introduction
- Electromagnetic Radius Calibration
 - Process Sequence
 - Results
 - Summary
- Electromagnetic Forming in the Flange
 - Process Analysis
 - Results
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Introduction

Motivation: Increased design freedom in deep drawing

Problem:

→ min. edge radius

→ max. drawing ratio $\beta_{\max} = \frac{r_0}{r_P}$

→ max. drawing depth h_{\max}



Bottom tear at a cylindrical cup

Introduction

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Problem:

→ min. edge radius

→ max. drawing ratio $\beta_{\max} = \frac{r_0}{r_P}$

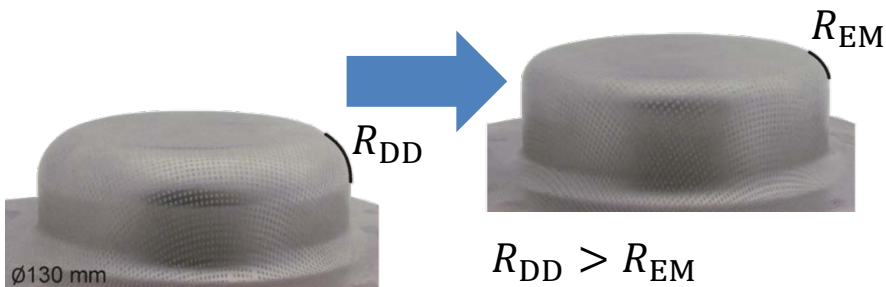
→ max. drawing depth h_{\max}



Bottom tear at a cylindrical cup

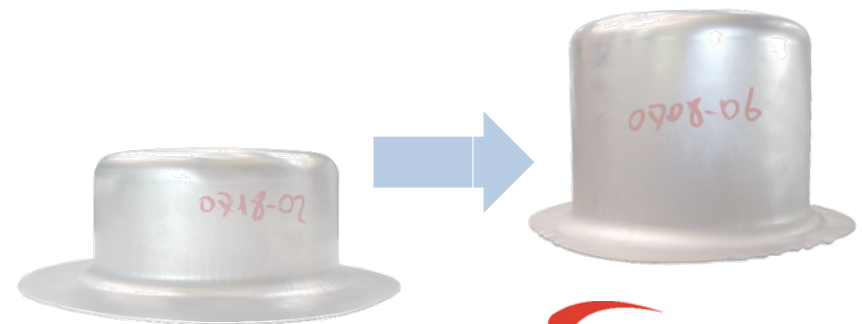
Electromagnetic Radius Calibration

→ Decreasing min. edge radius



Electromagnetic Forming in the Flange

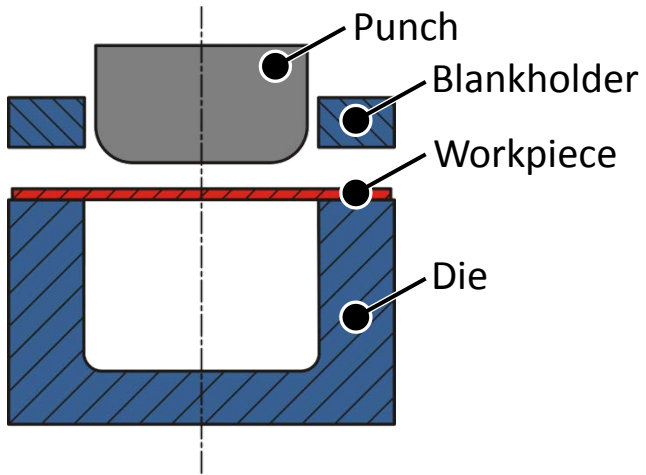
→ Increasing β_{\max} and h_{\max}



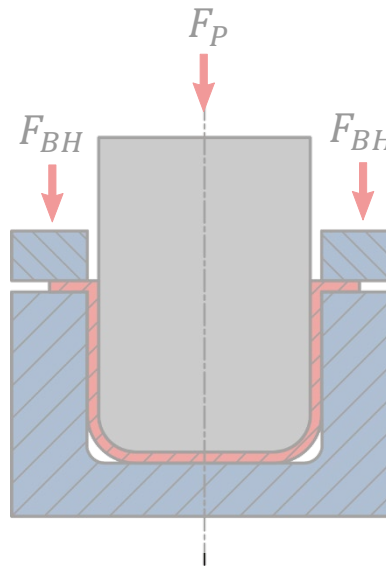
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Electromagnetic Radius Calibration

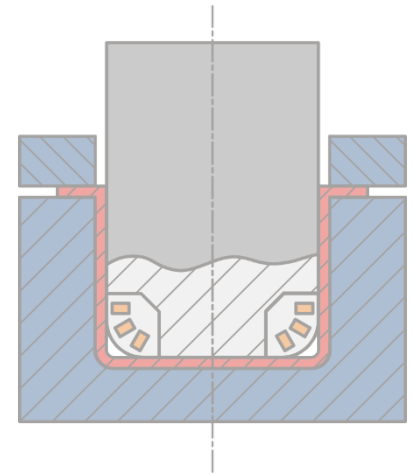
Process sequence



1. Deep drawing

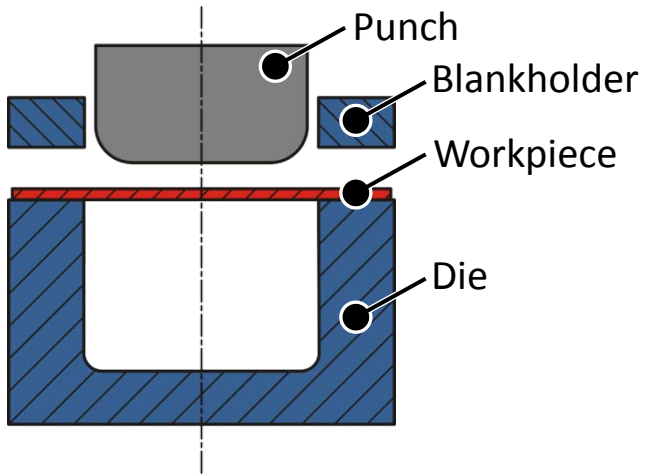


2. EM Calibration

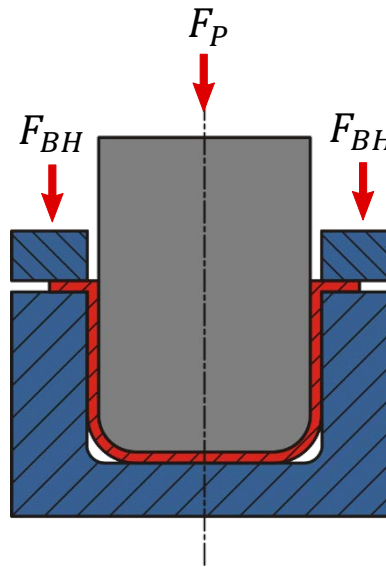


Electromagnetic Radius Calibration

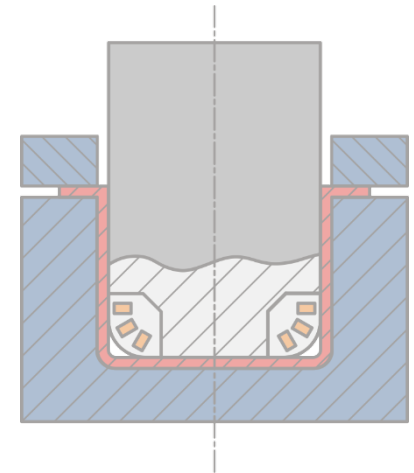
Process sequence



1. Deep drawing



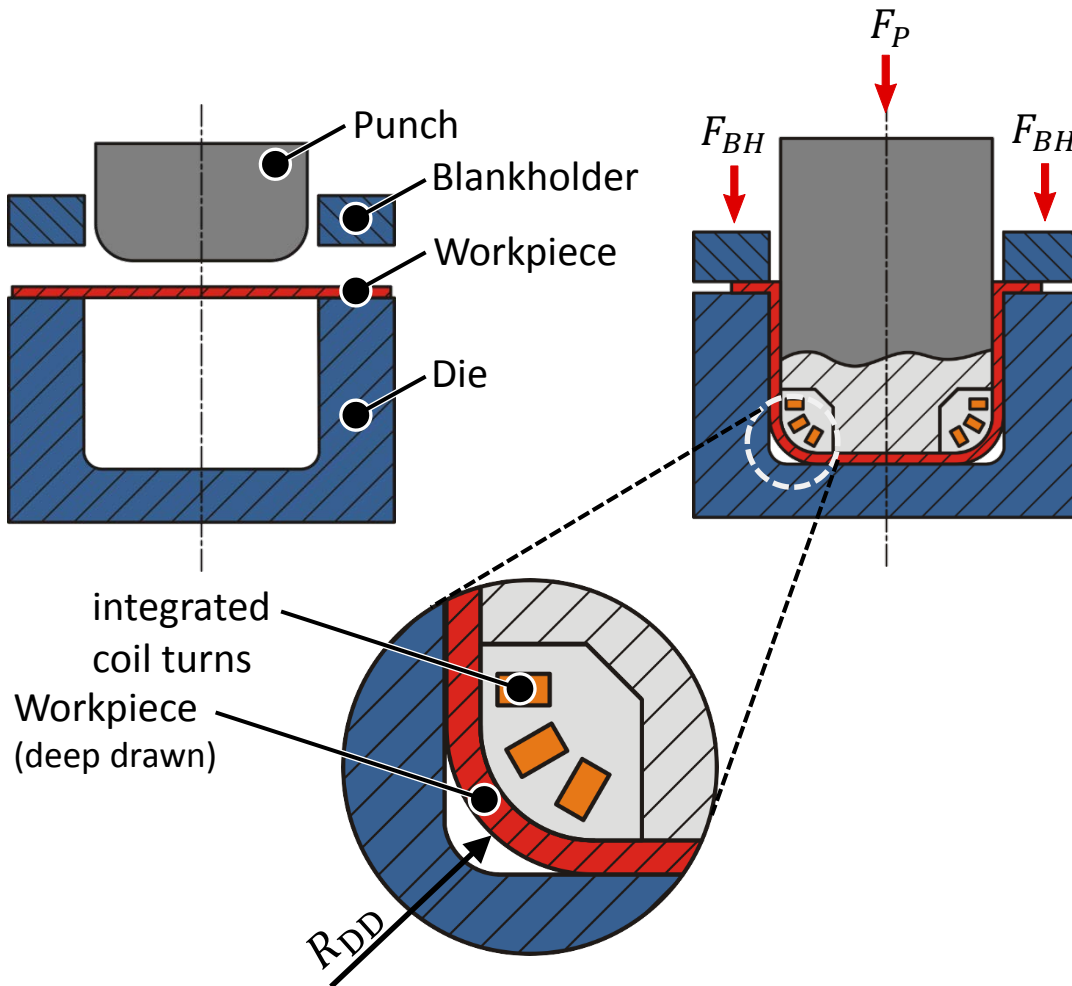
2. EM Calibration



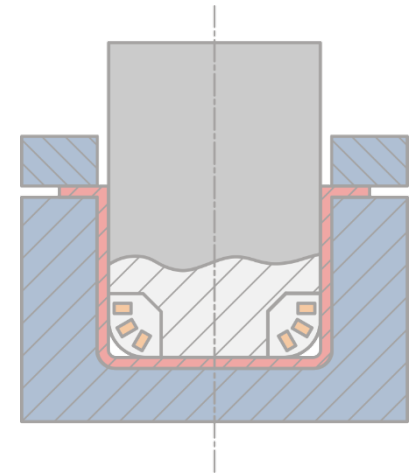
Electromagnetic Radius Calibration

Process sequence

1. Deep drawing

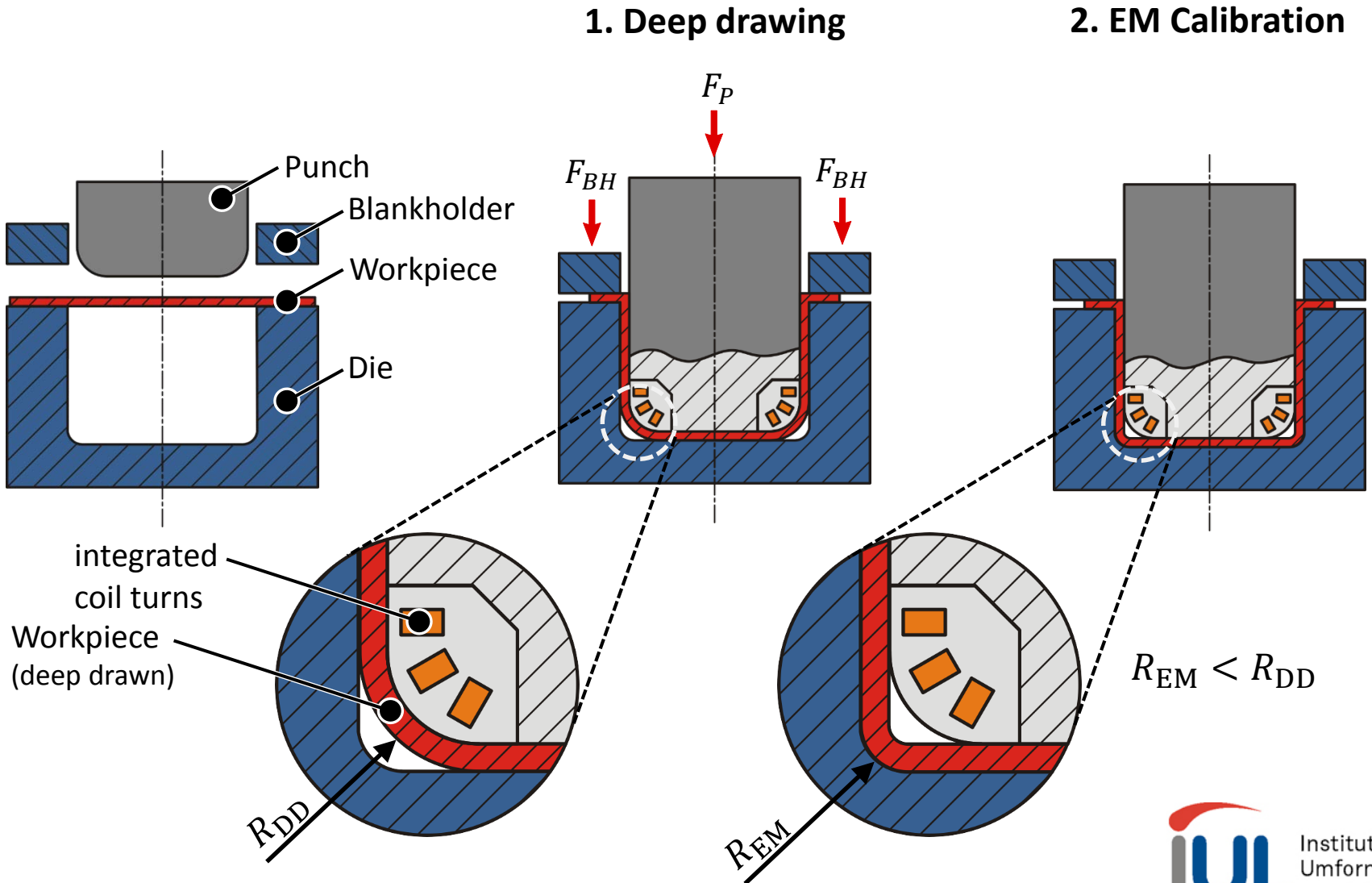


2. EM Calibration



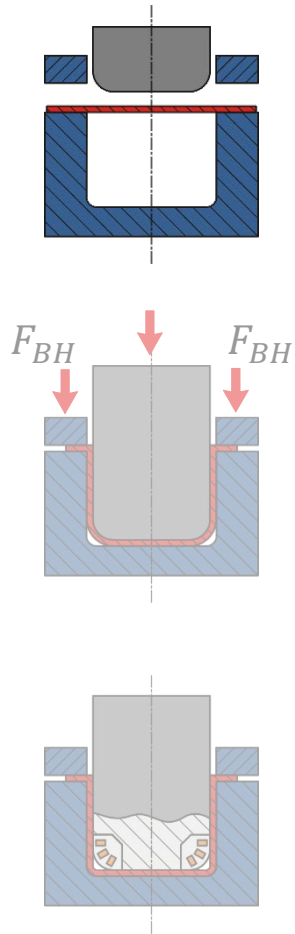
Electromagnetic Radius Calibration

Process sequence

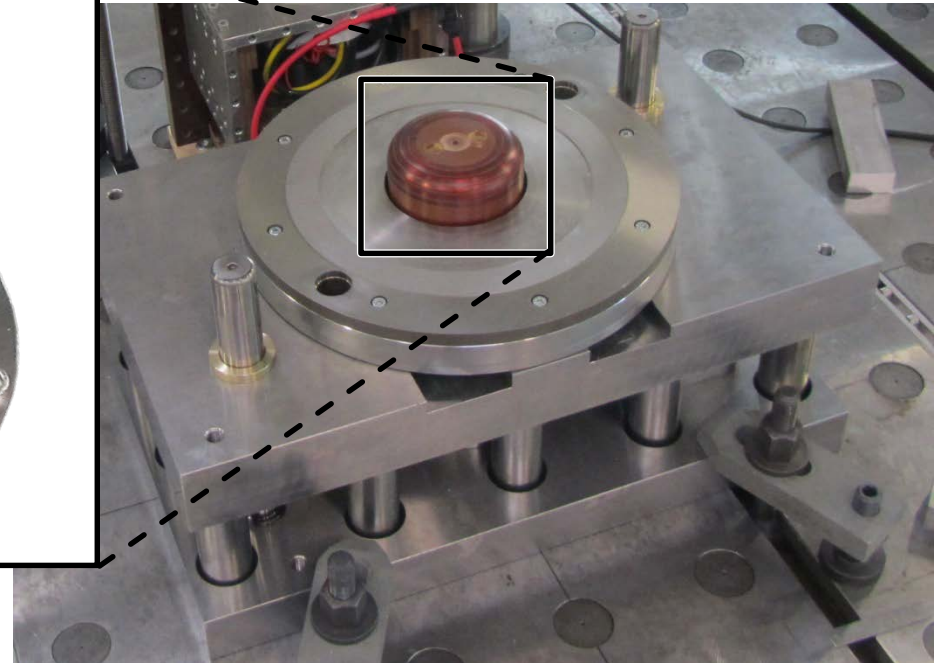


Electromagnetic Radius Calibration

Setup and Procedure



Punch with integrated coil turns



Deep drawing:

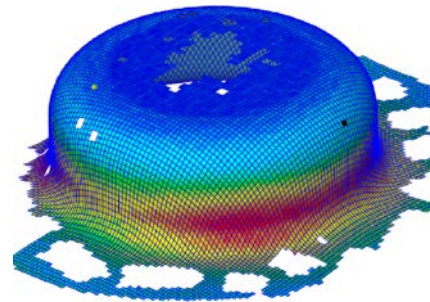
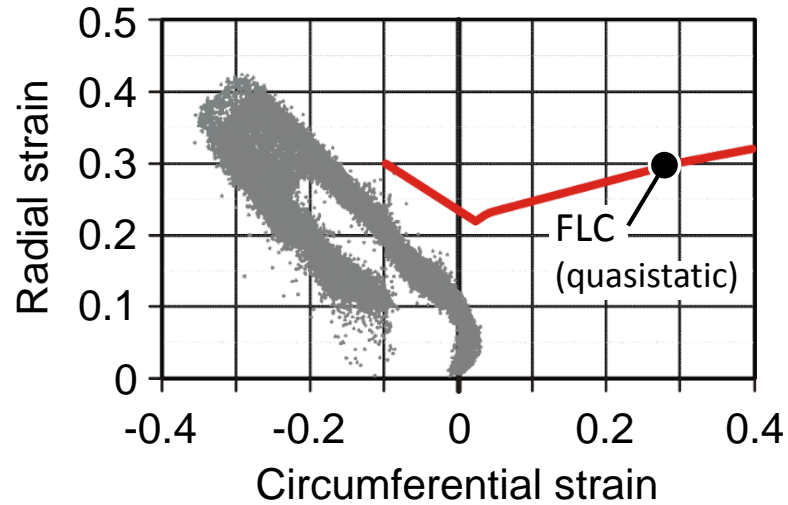
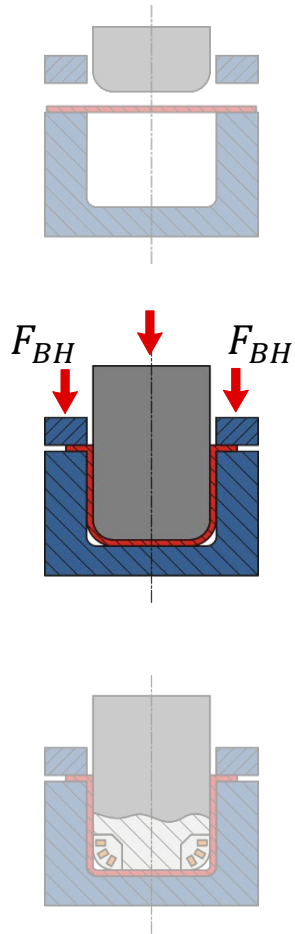
Punch diameter: 130 mm
Punch edge radius: 20 mm
Die radius: 10 mm

Workpiece:

Material EN AW-5083
Geometry t=1 / Ø260 mm
Yield stress 150 MPa

Electromagnetic Radius Calibration

Results: After deep drawing



Strain distribution
after deep-drawing

$$R_{DD} = 21 \text{ mm}$$

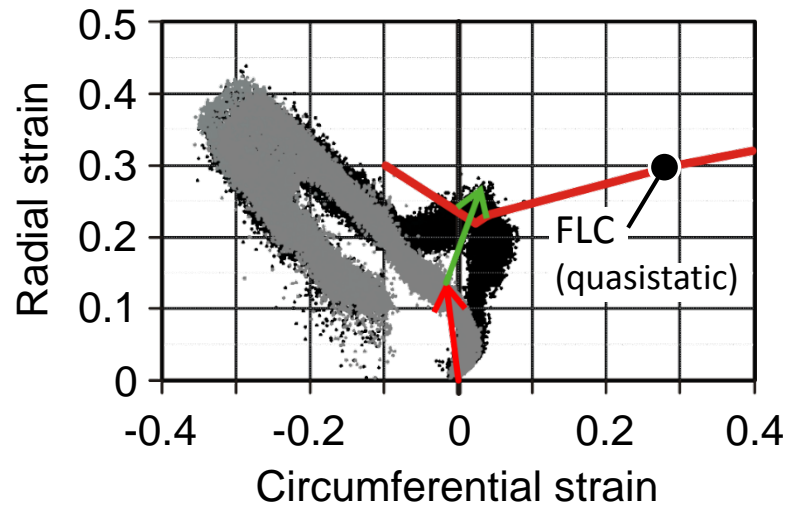
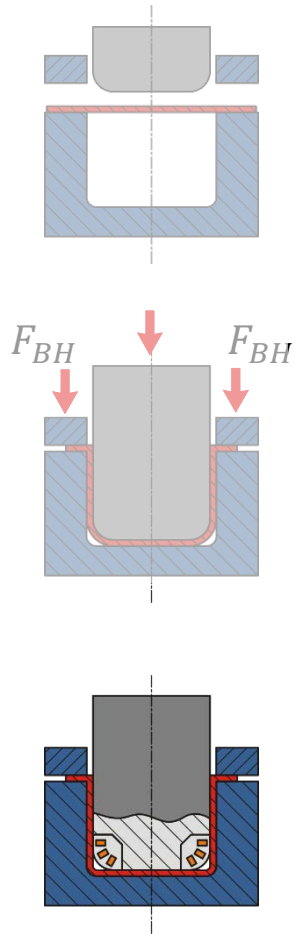
Punch/Sheet:
no lubrication

Flange/Sheet:
excessive lubrication

Blankholder force:
 $F_{BH} = 740 \text{ kN}$

Electromagnetic Radius Calibration

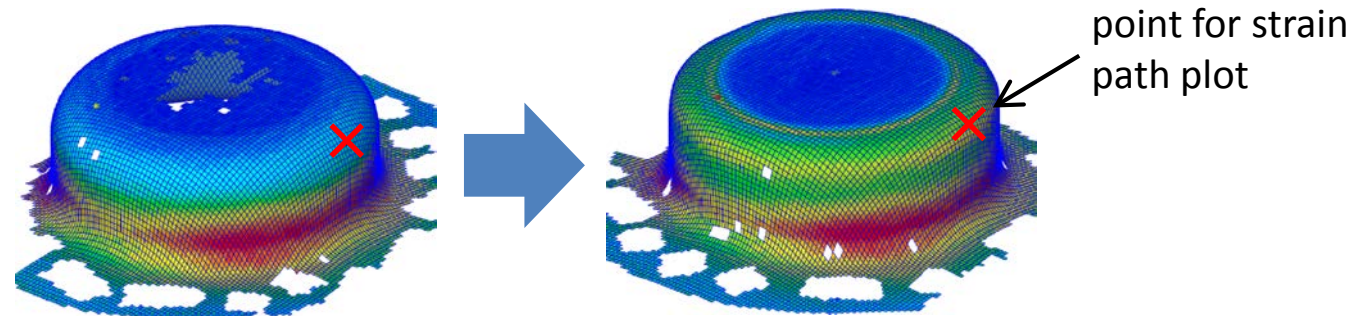
Results: After EM-Calibration



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Strain distribution
after deep-drawing

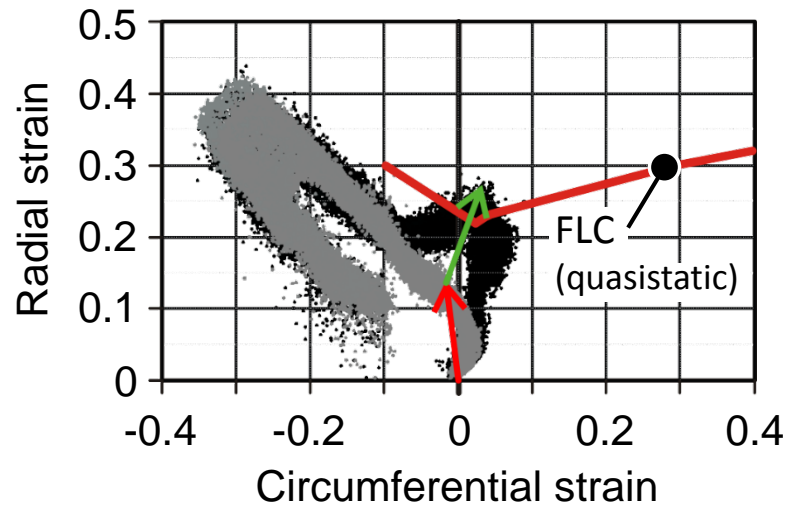
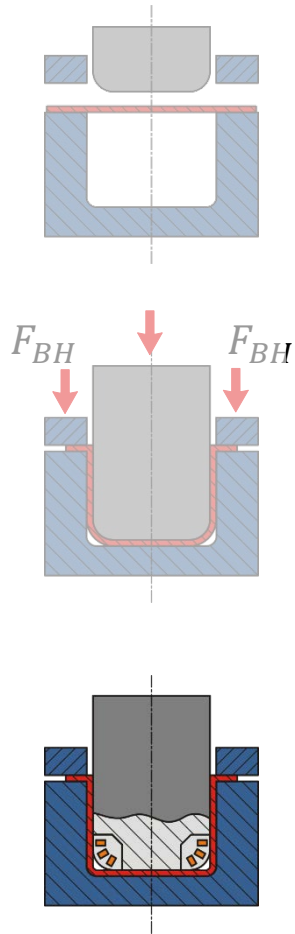
$R_{DD} = 21 \text{ mm}$

Strain distribution
after EM-Calibration

$R_{EM} = 13 \text{ mm}$

Electromagnetic Radius Calibration

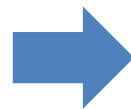
Results: After EM-Calibration



Punch/Sheet:
no lubrication

Flange/Sheet:
excessive lubrication

Blankholder force:
 $F_{BH} = 740 \text{ kN}$

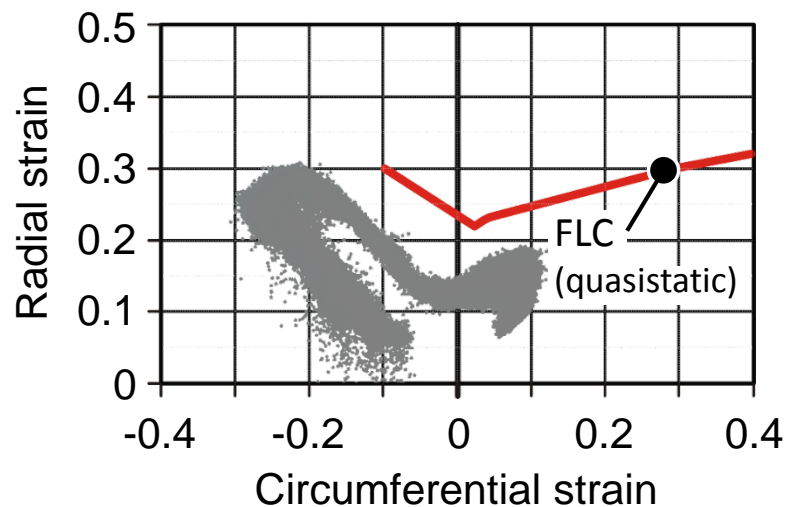
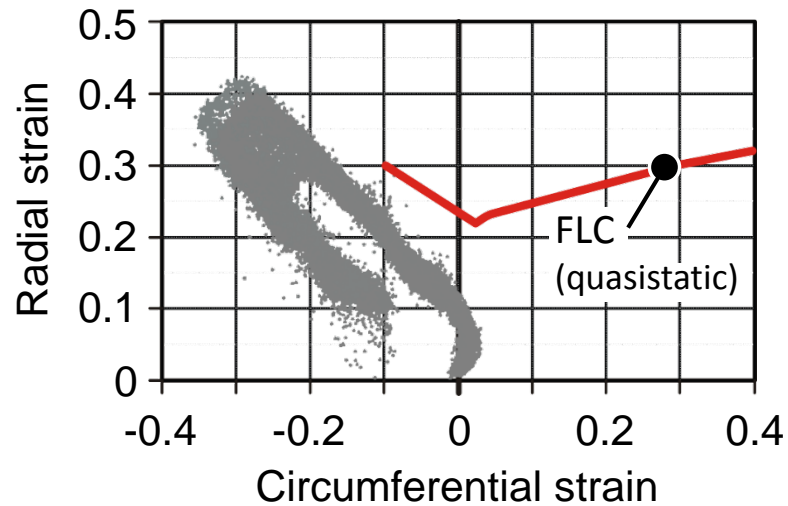
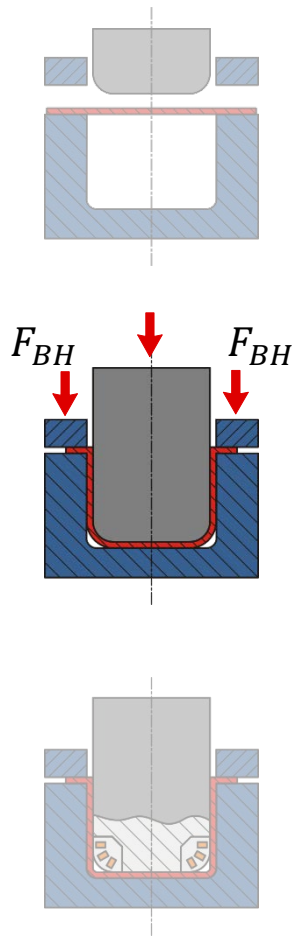


Requirements for increased forming limit:

- Strain rate change?
- Strain path change?
- Amount of prestraining?

Electromagnetic Radius Calibration

Results: After deep drawing



Punch/Sheet:
no lubrication

Flange/Sheet:
excessive lubrication

Blankholder force:
 $F_{BH} = 740$ kN

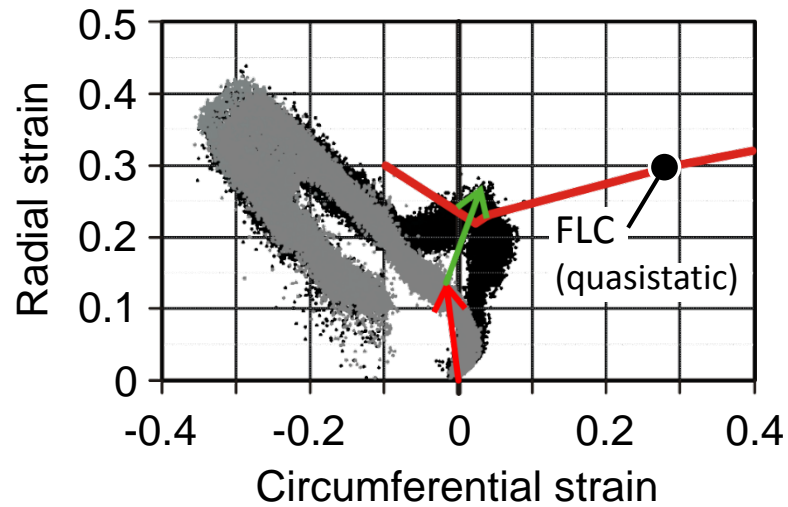
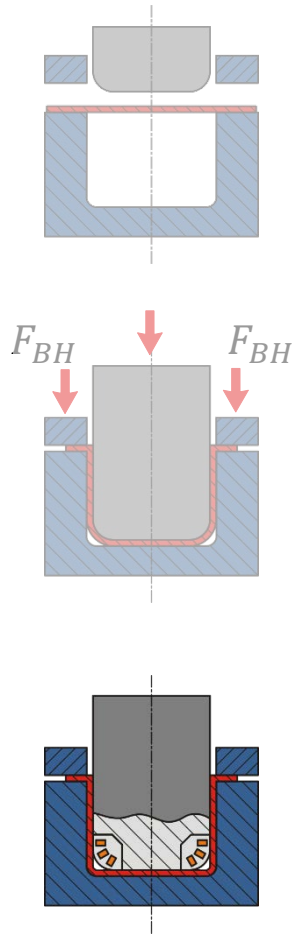
Punch/Sheet:
excessive lubrication

Flange/Sheet:
no lubrication

Blankholder force:
 $F_{BH} = 520$ kN

Electromagnetic Radius Calibration

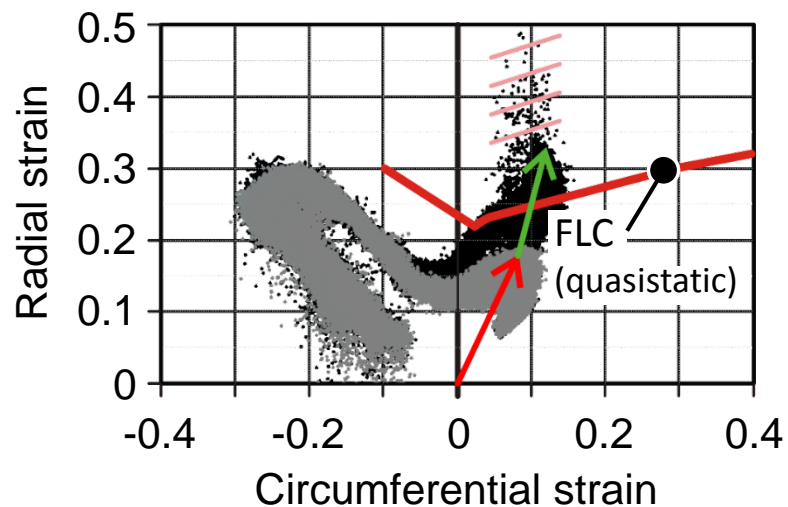
Results: After EM-Calibration



Punch/Sheet:
no lubrication

Flange/Sheet:
excessive lubrication

Blankholder force:
 $F_{BH} = 740 \text{ kN}$



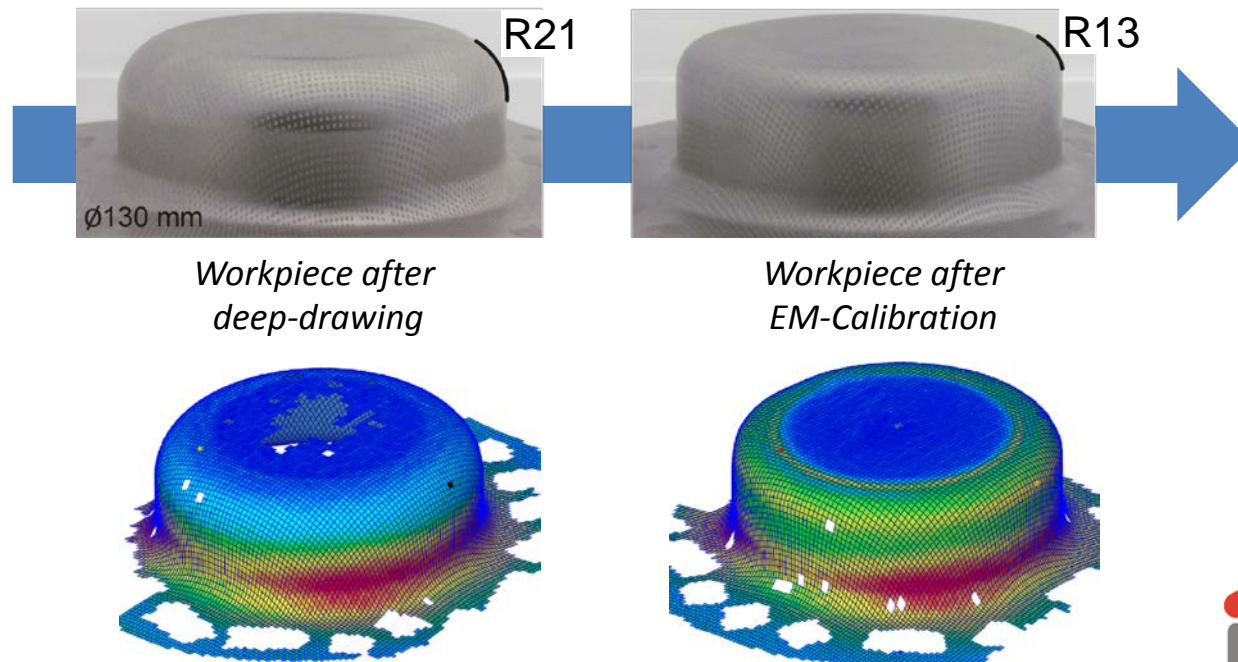
Punch/Sheet:
excessive lubrication

Flange/Sheet:
no lubrication

Blankholder force:
 $F_{BH} = 520 \text{ kN}$

Electromagnetic Radius Calibration

- Increased forming limit
- Decreased cup radius ($R_{DD} = 21\text{mm} \rightarrow R_{EM} = 13\text{mm}$)
- Mainly caused by strain-rate change
- No strain-path change required
- No remaining quasi-static forming limit required



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Introduction

Motivation: Increased design freedom

Problem:

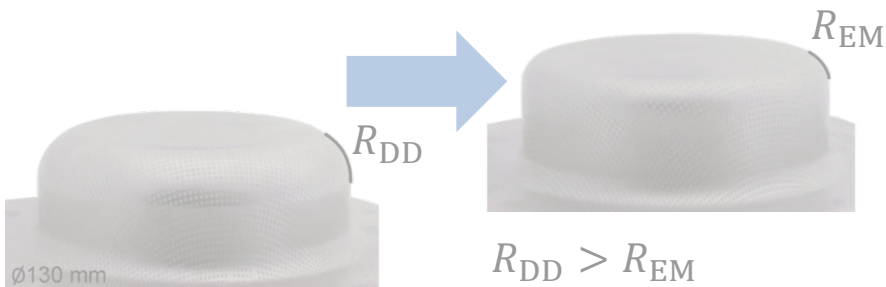
- min. edge radius
- max. drawing ratio $\beta_{\max} = \frac{r_0}{r_P}$
- max. drawing depth h_{\max}



Bottom tear at a cylindrical cup

Electromagnetic Radius Calibration

→ Decreasing min. edge radius



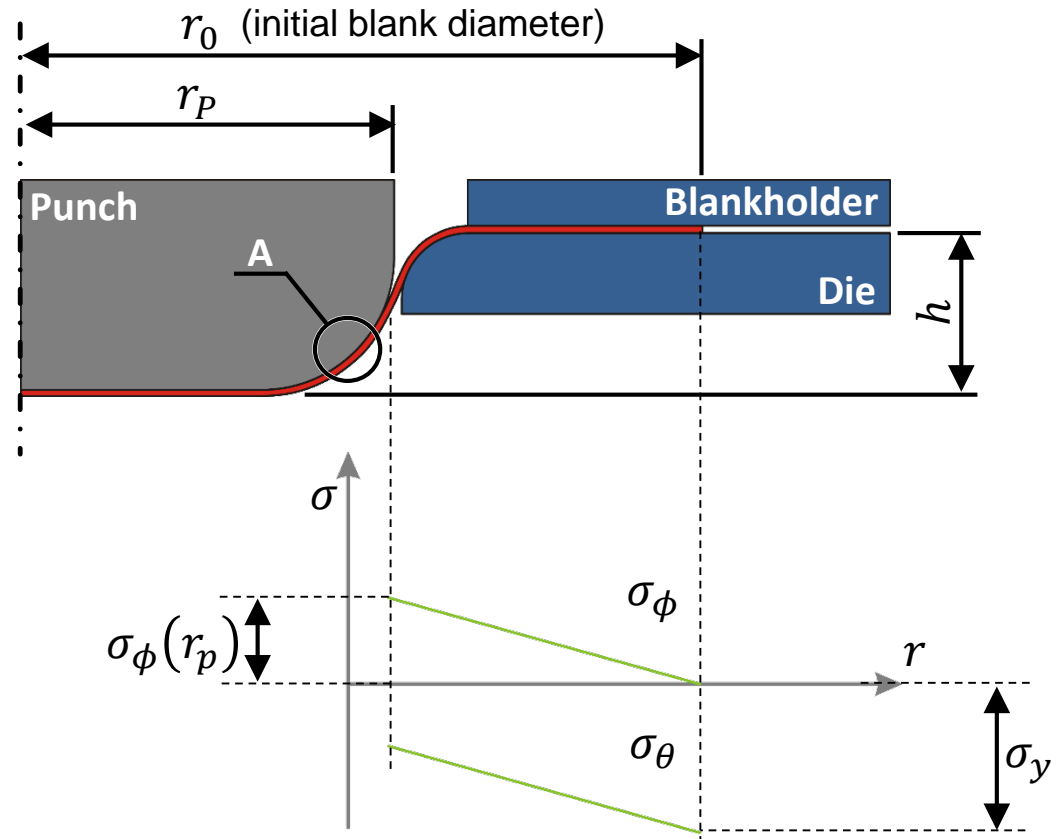
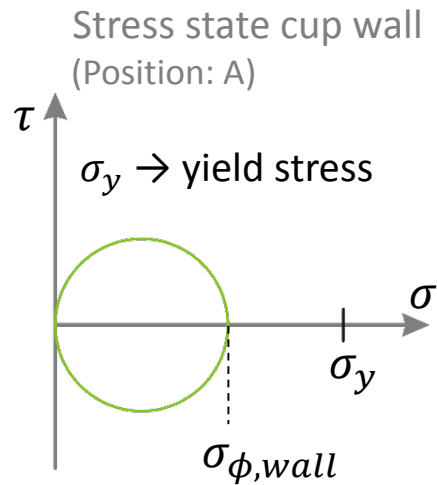
Electromagnetic Forming in the Flange

→ Increasing β_{\max} and h_{\max}



Electromagnetic Forming in the Flange

Process analysis: Failure mechanism



$$\sigma_{\phi}(r_p) = \sigma_{\phi,wall}$$

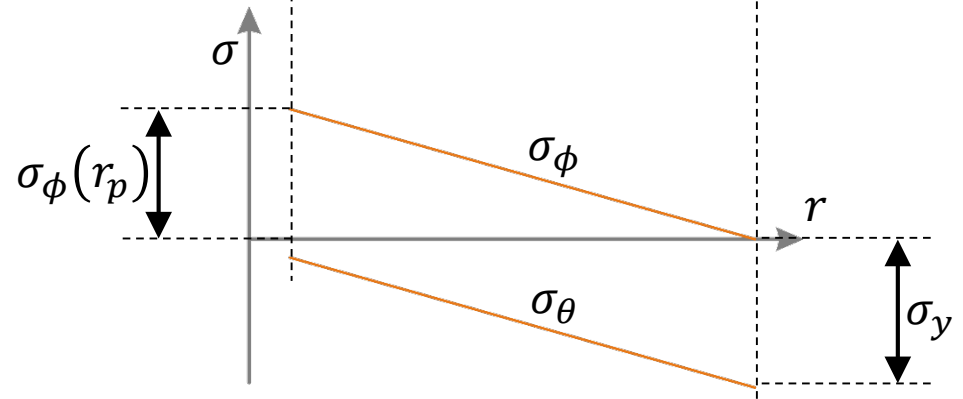
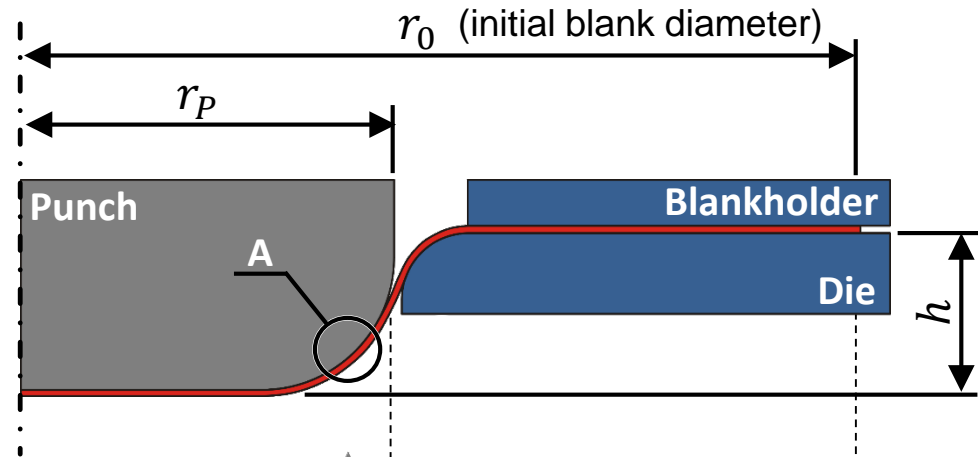
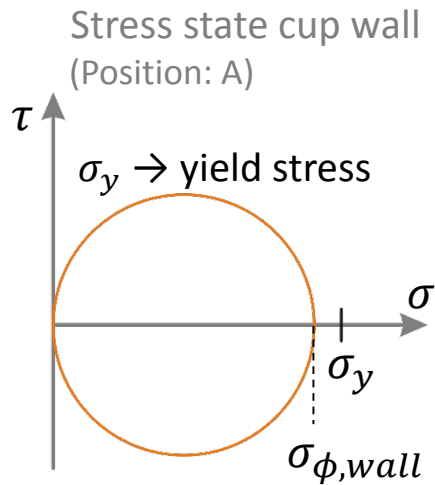
$$\sigma_{\phi}(r_p) = \sigma_y \cdot \ln(\beta)$$

$$\beta = r_0 / r_p$$

(no friction, no work hardening)

Electromagnetic Forming in the Flange

Process analysis: Failure mechanism



$$\beta > \beta_{max}$$

$$\sigma_{\phi,wall} = \sigma_y$$

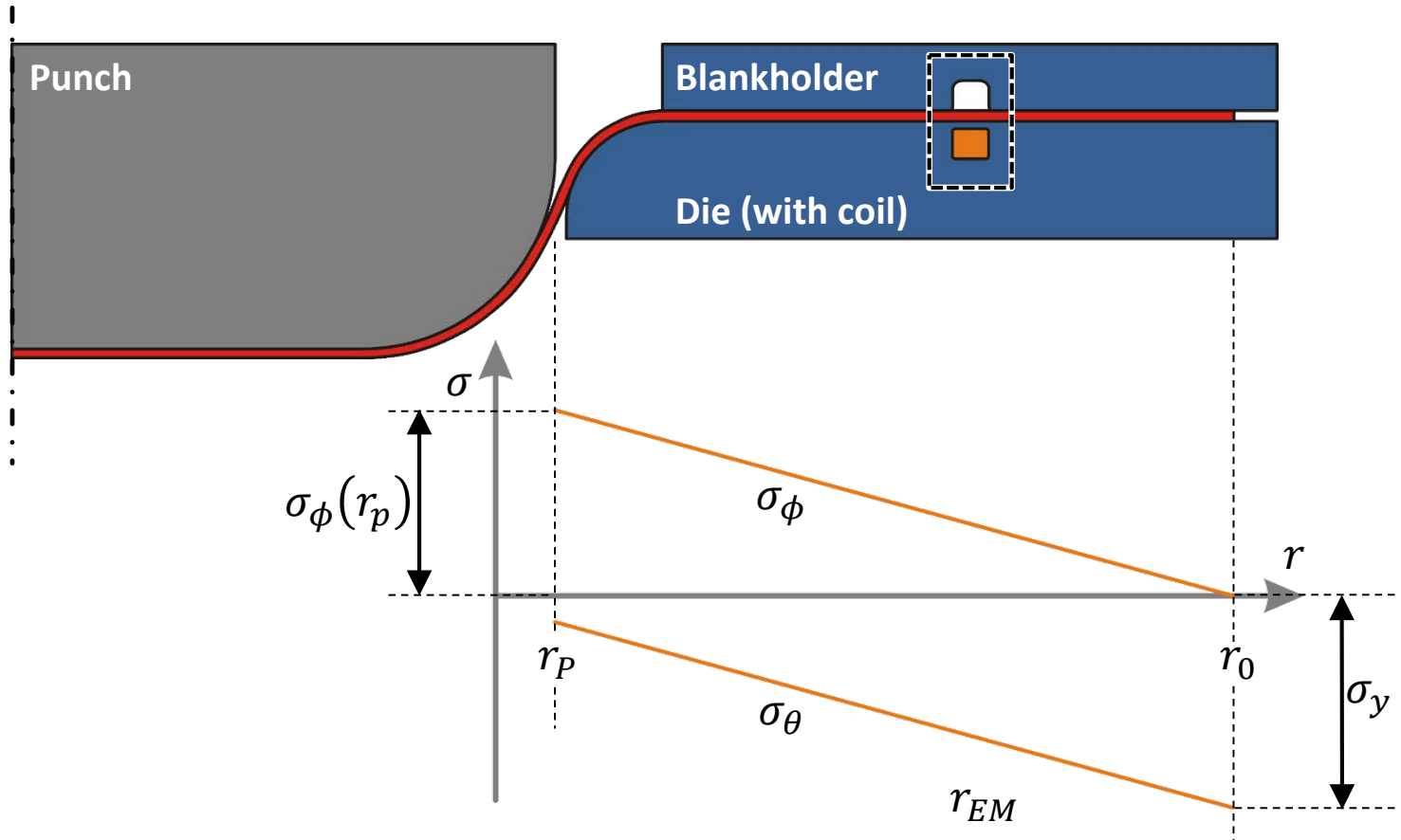
Bottom tearing



Electromagnetic Forming in the Flange

Process analysis: Reduction of meridional stresses

➔ EM bulge forming in the flange*¹

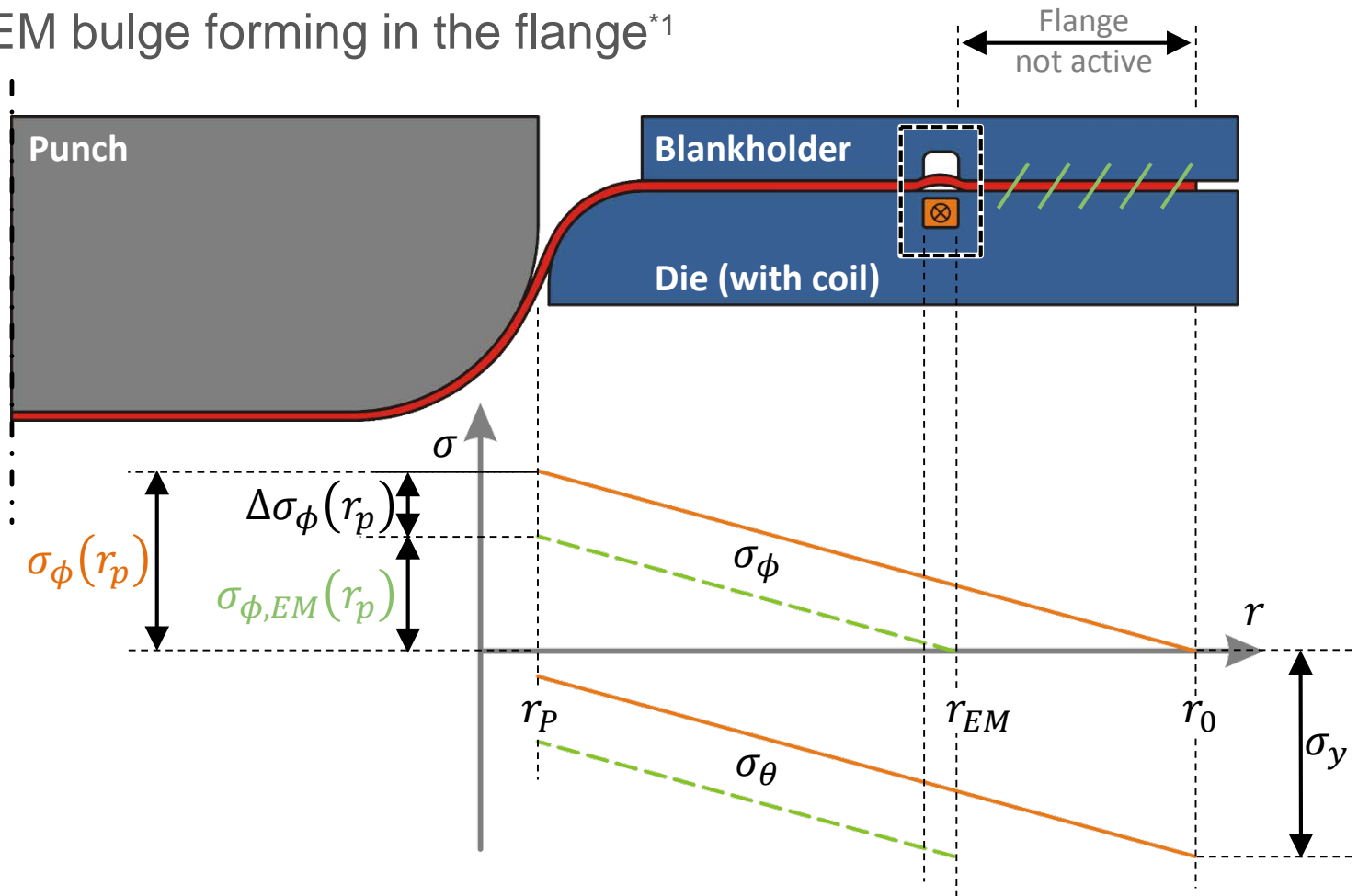


*¹ Shang, J.: *Electromagnetically Assisted Sheet Metal Stamping*, 2006

Electromagnetic Forming in the Flange

Process analysis: Reduction of meridional stresses

➔ EM bulge forming in the flange*¹

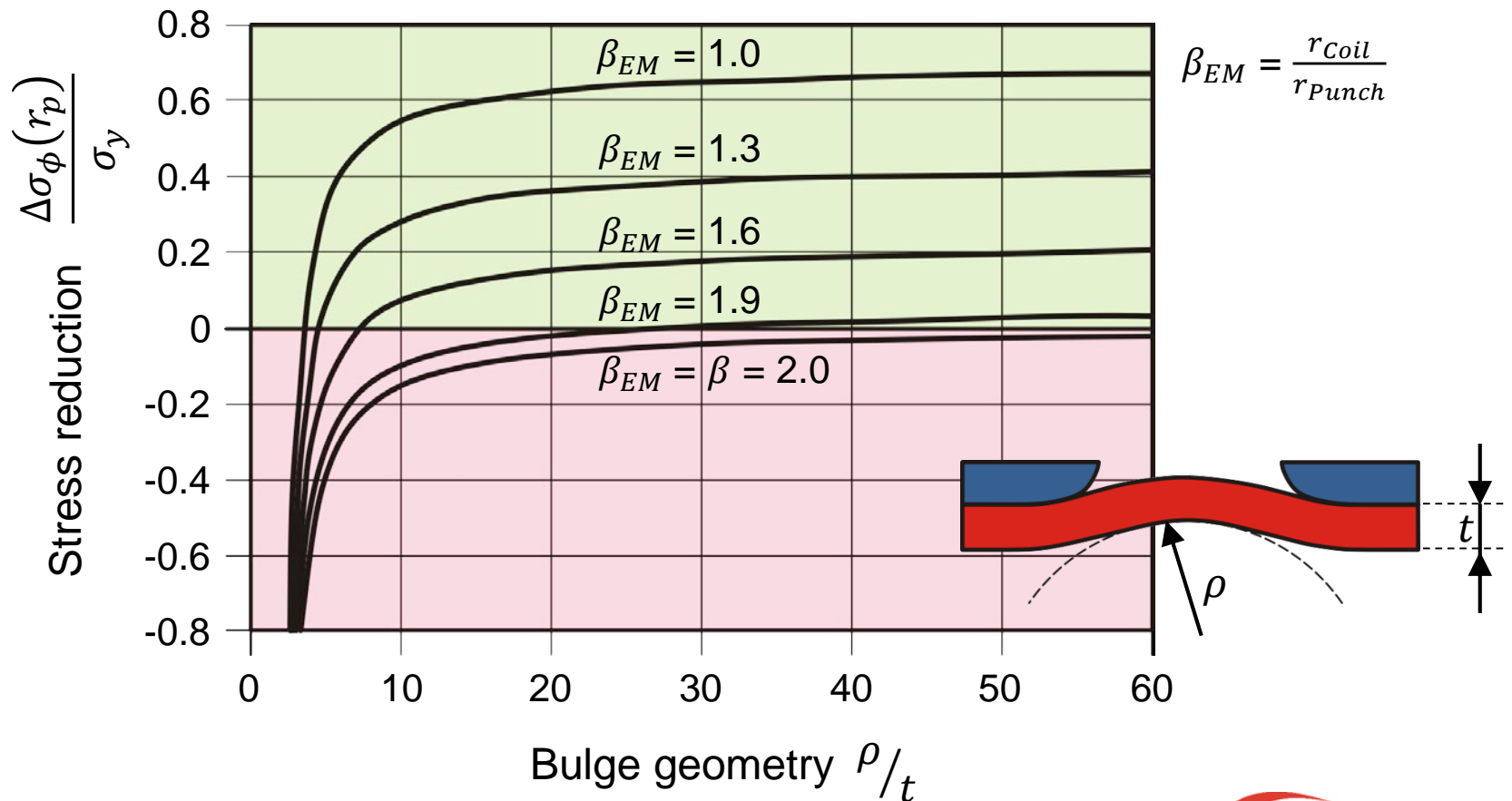


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Electromagnetic Forming in the Flange

Process analysis: Reduction of meridional stresses

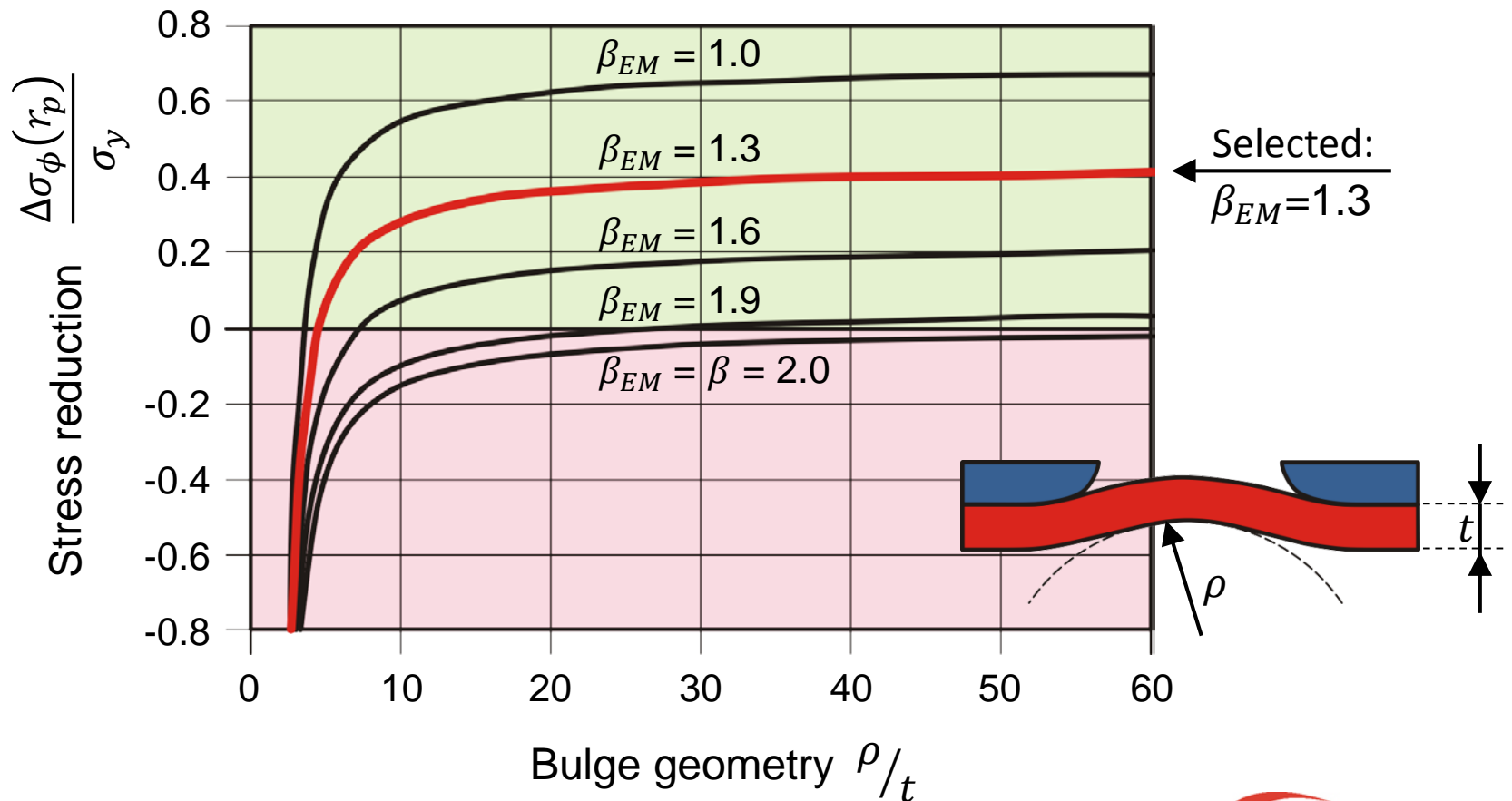
➔ Derivation of coil position



Electromagnetic Forming in the Flange

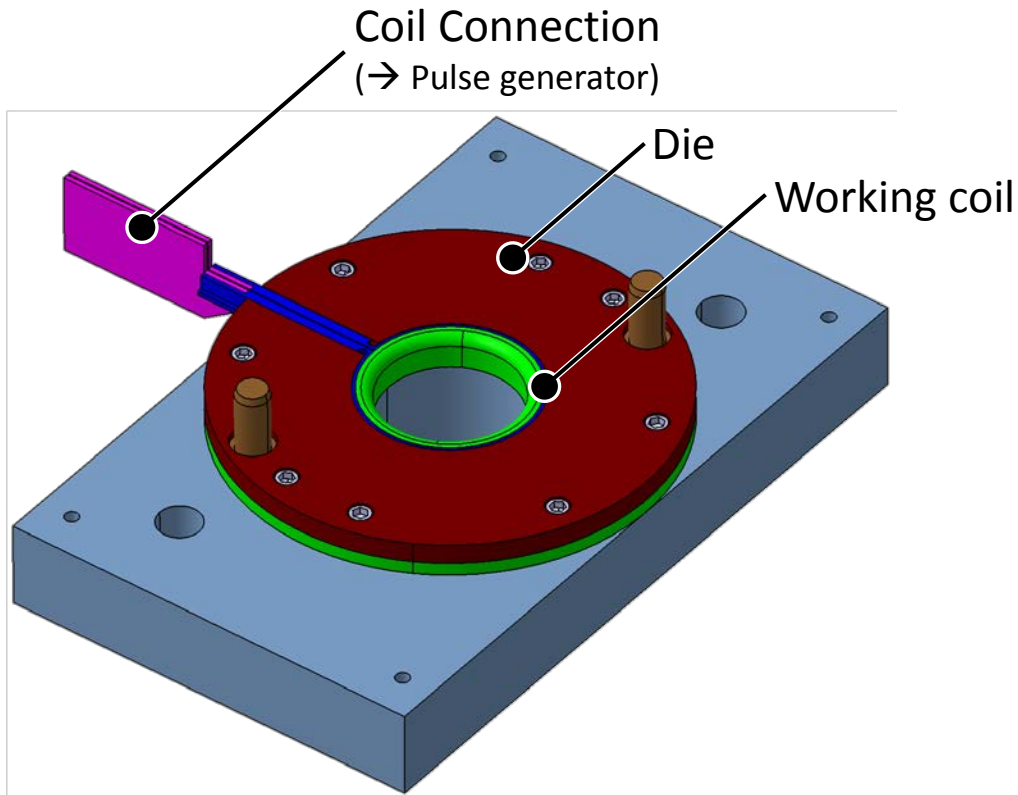
Process analysis: Reduction of meridional stresses

➔ Derivation of coil position



Electromagnetic Forming in the Flange

Setup and Procedure



Deep drawing

Punch diameter: 130 mm

Punch radius: 20 mm

Die radius: 10 mm

Electromagnetic forming

Coil diameter: 162 mm (inner)

Coil turn width: 3.35 mm

Pulse generator: Maxwell 7000

$R_i = 3.3 \text{ m}\Omega$

$L_i = 50 \text{ nH}$

$C = 992 \text{ }\mu\text{F}$

Workpiece:

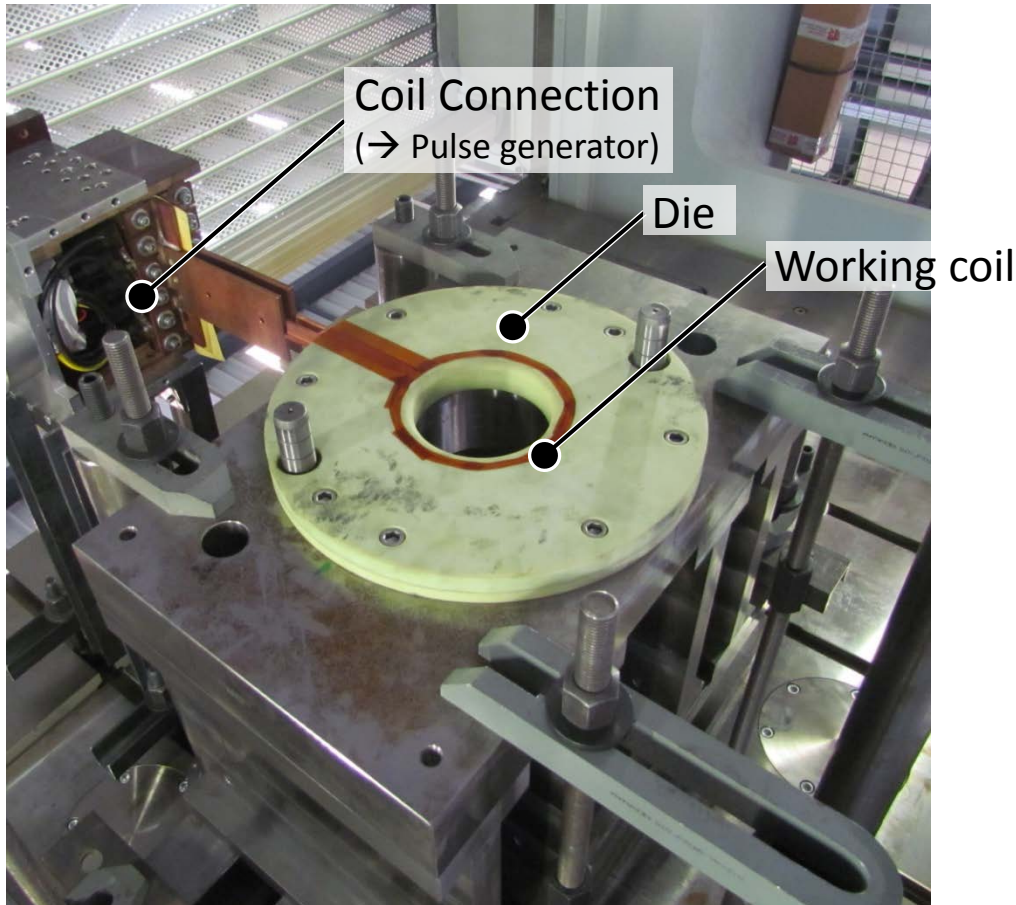
Material EN AW-5083

Sheet thickness 1mm

Yield stress 150 MPa

Electromagnetic Forming in the Flange

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Results: Overview

1. Limit of conventional deep drawing $\rightarrow \beta_{\max} = 2.0$

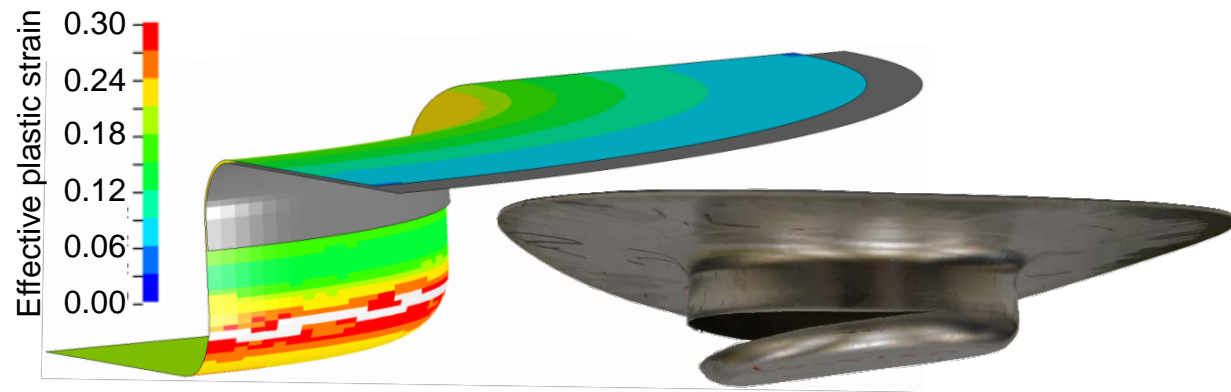


Figure: Material failure in simulation and experiment ($\beta=2.1$)

Results: Overview

1. Limit of conventional deep drawing $\rightarrow \beta_{\max} = 2.0$

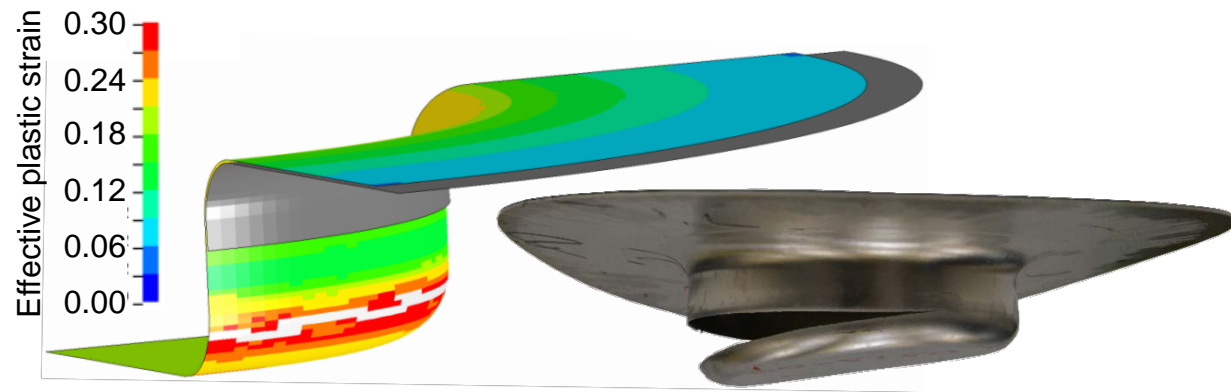
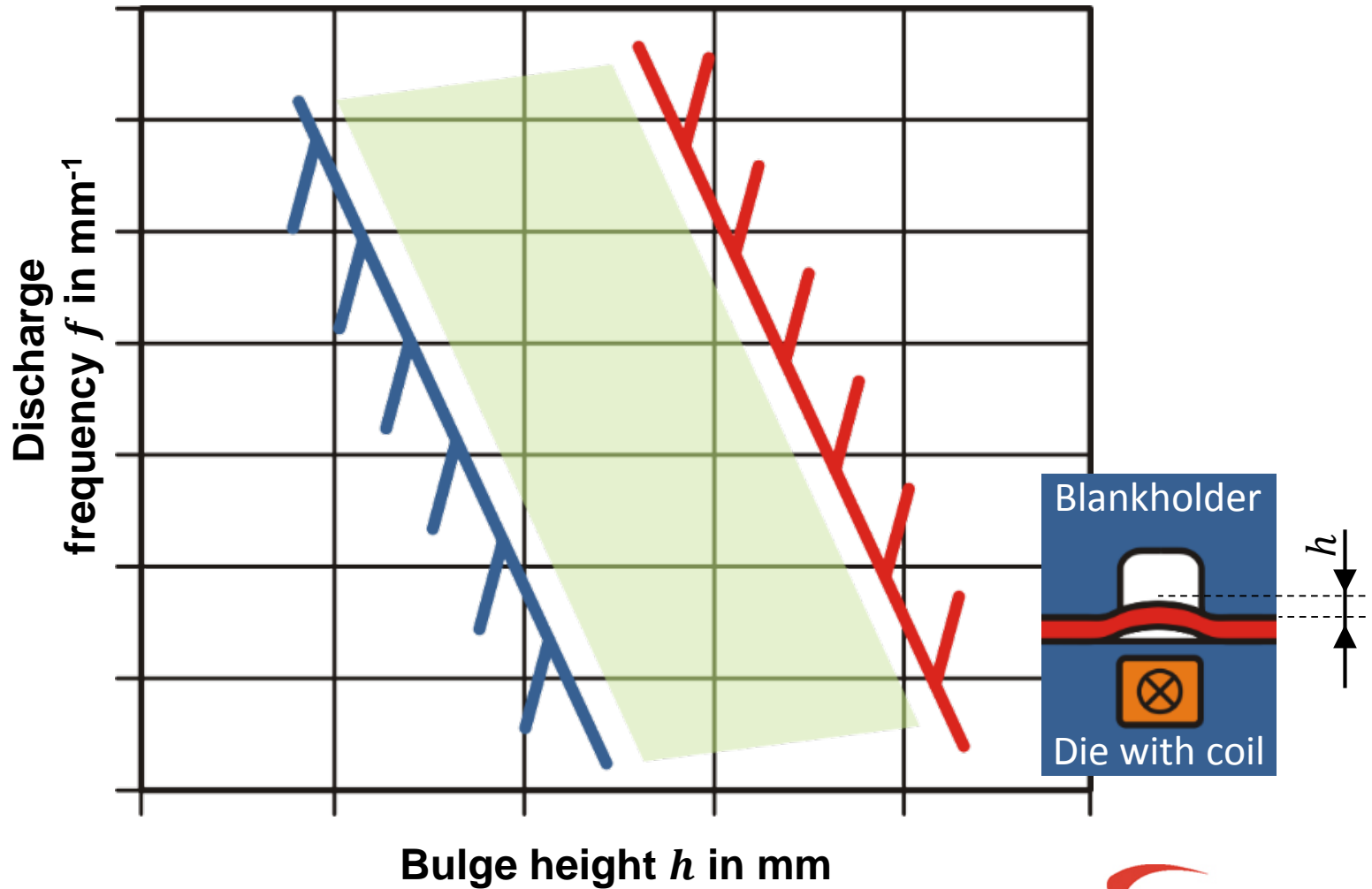


Figure: Material failure in simulation and experiment ($\beta=2.1$)

2. Process window for EM-assisted deep drawing

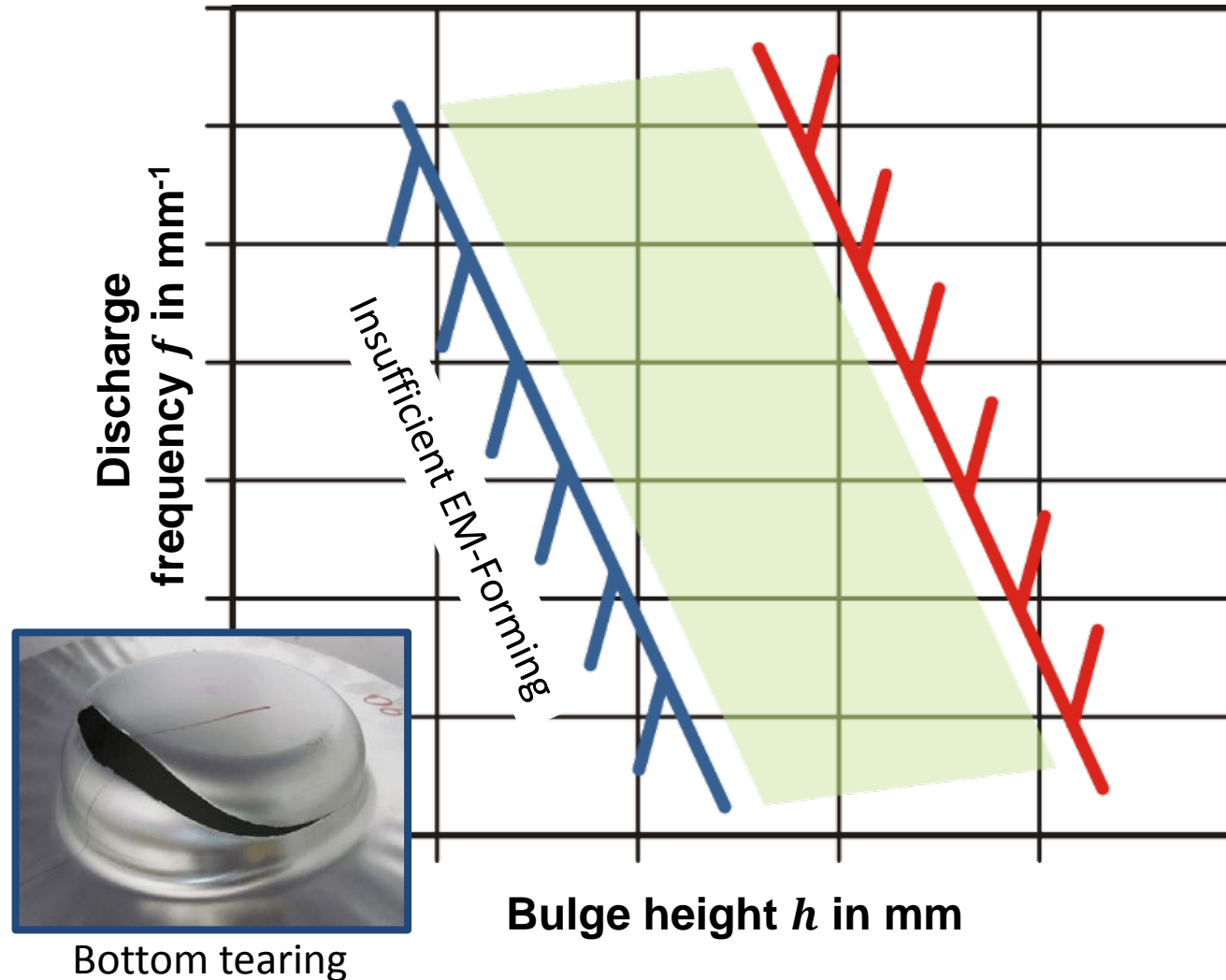
Electromagnetic Forming in the Flange

Results: Determination of process window



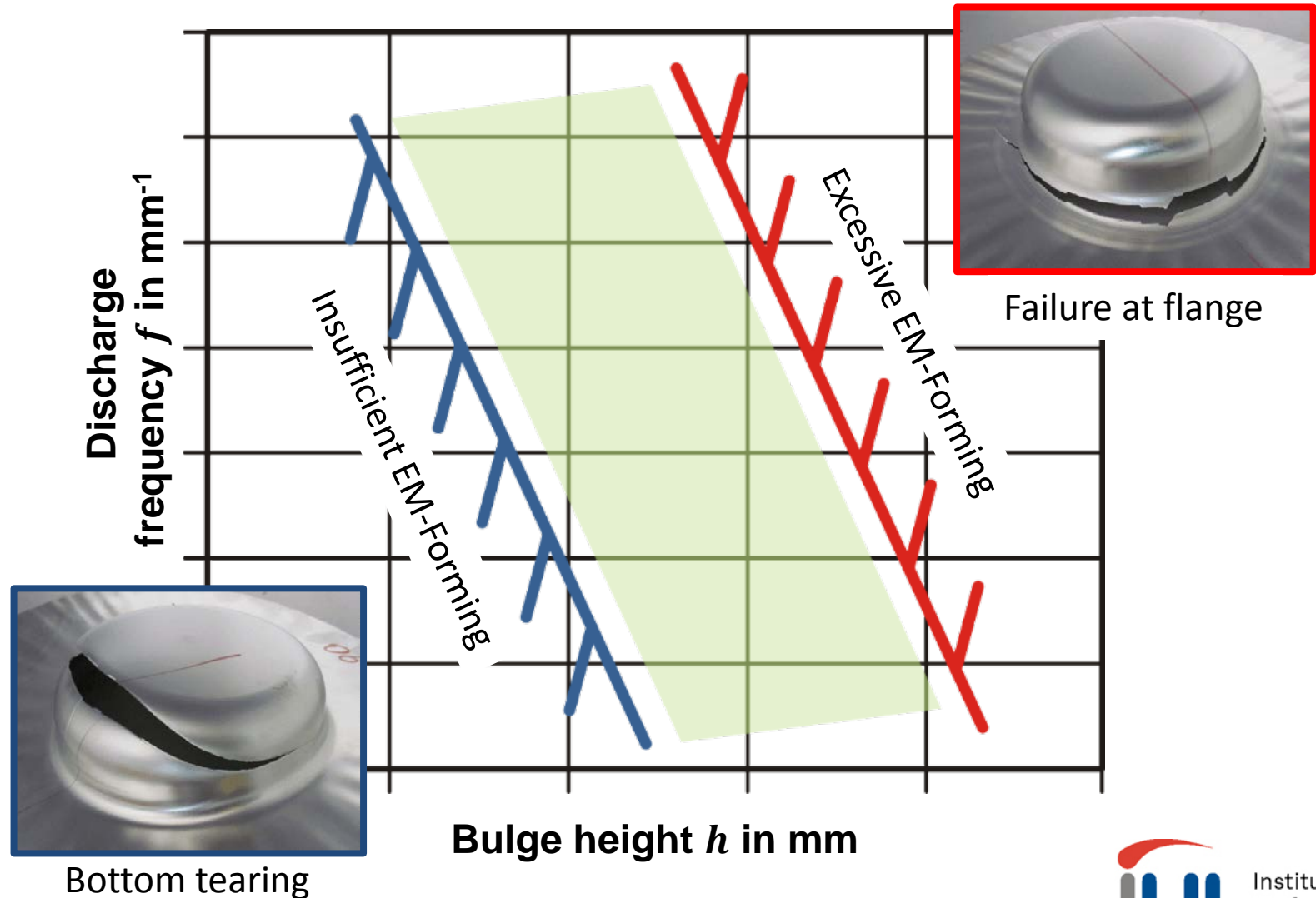
Electromagnetic Forming in the Flange

Results: Determination of process window



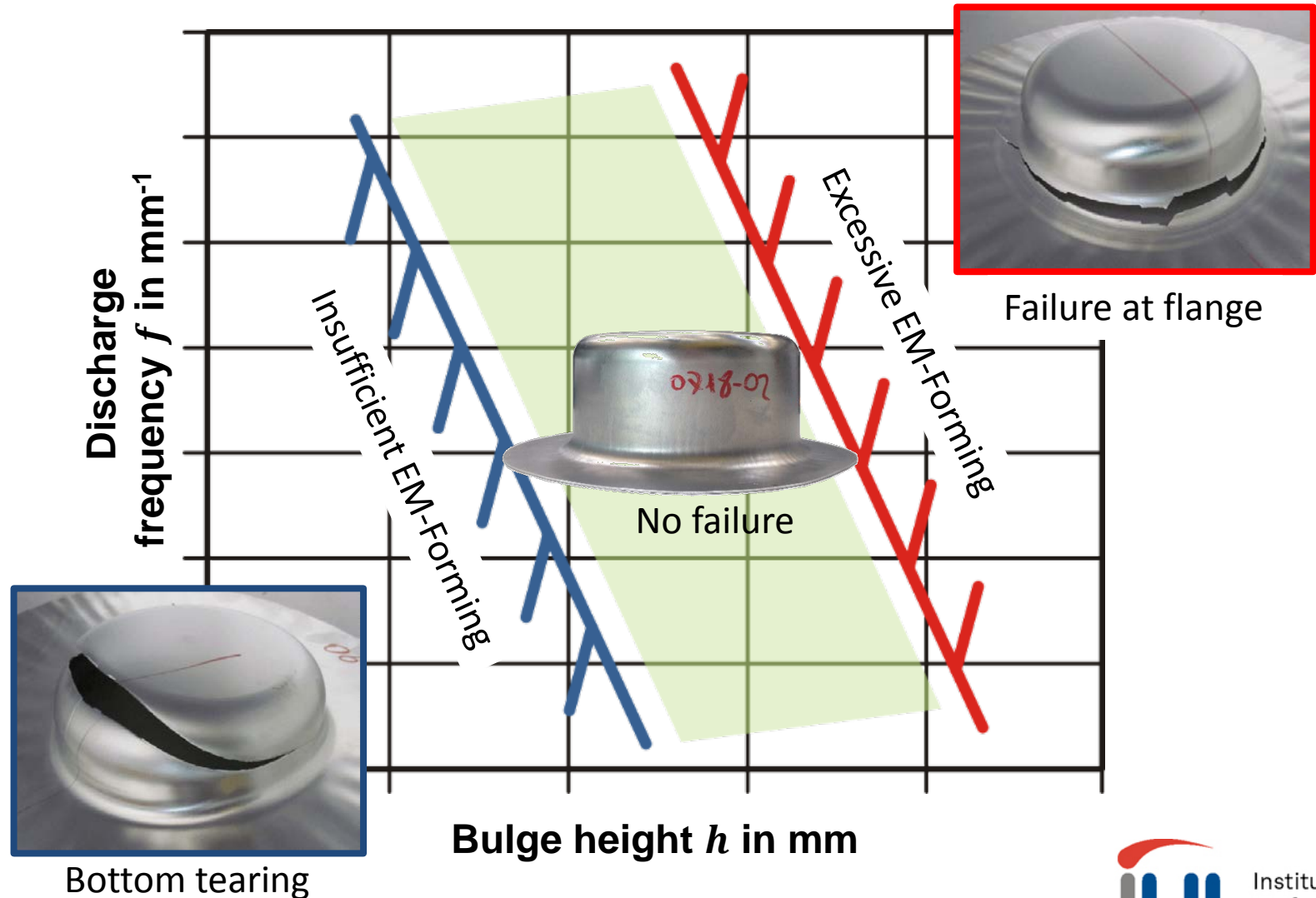
Electromagnetic Forming in the Flange

Results: Determination of process window



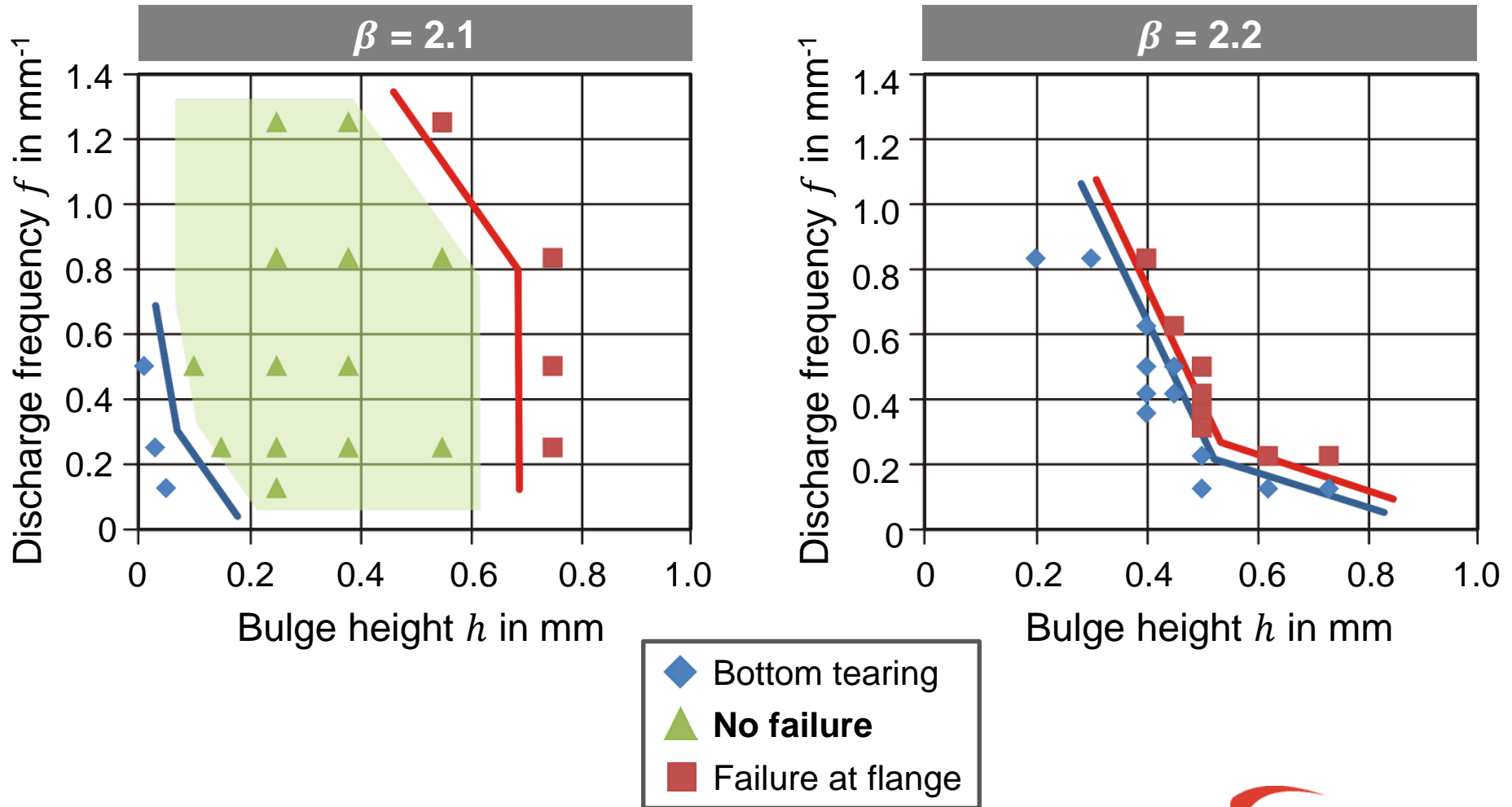
Electromagnetic Forming in the Flange

Results: Determination of process window



Electromagnetic Forming in the Flange

Results: Determination of process window



Electromagnetic Forming in the Flange

Results: Overview

1. Limit of conventional deep drawing $\rightarrow \beta_{\max} = 2.0$

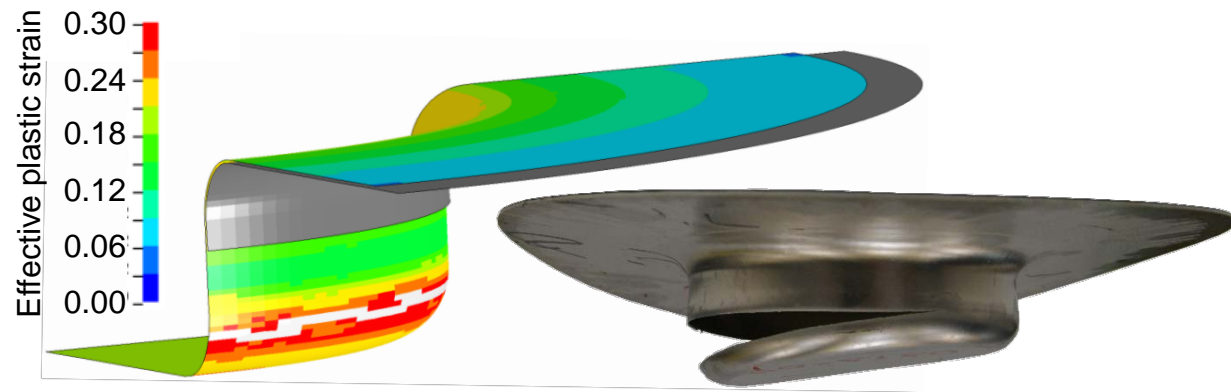


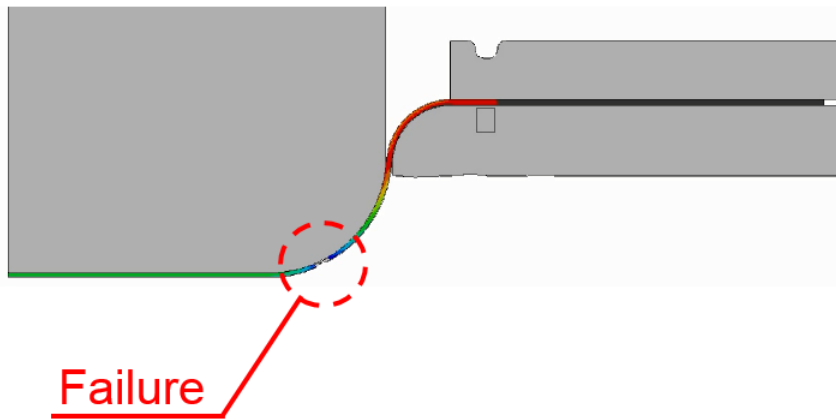
Figure: Material failure in simulation and experiment ($\beta=2.1$)

2. Process window for EM-assisted deep drawing $\rightarrow \beta_{\max,EM} = 2.1$
3. Increase of the drawing depth h_{\max}

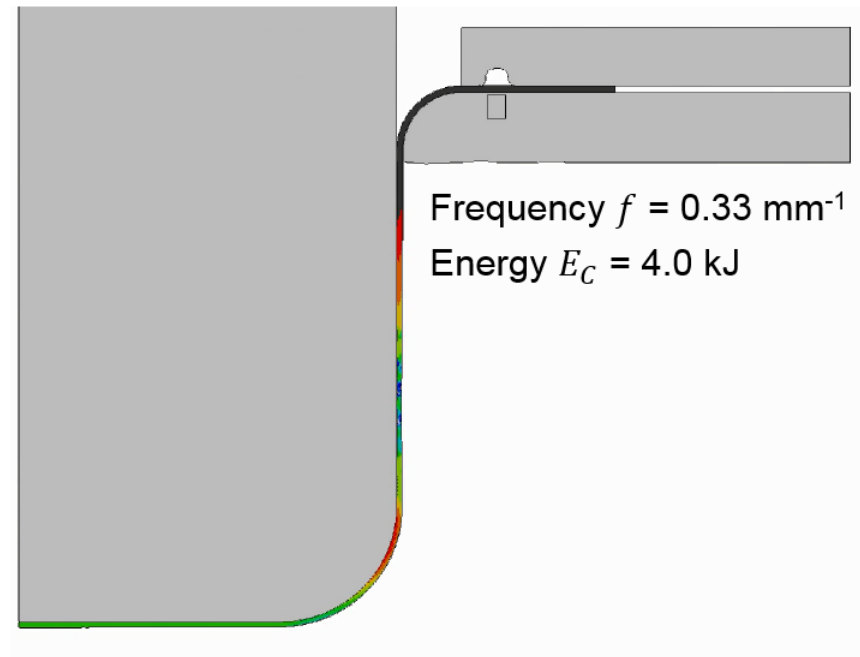
Electromagnetic Forming in the Flange

Results: Increase of the maximum drawing depth h_{\max}

Conventional deep drawing ($\beta=2.1$)



EM-assisted deep drawing ($\beta=2.1$)



$h_{\max} = 33 \text{ mm}$ ← $\beta^* = 2.2$ → $h_{\max,EM} = 57 \text{ mm (+73\%)}$

$h_{\max} = 36 \text{ mm}$ ← $\beta^* = 2.5$ → $h_{\max,EM} = 41 \text{ mm (+14\%)}$

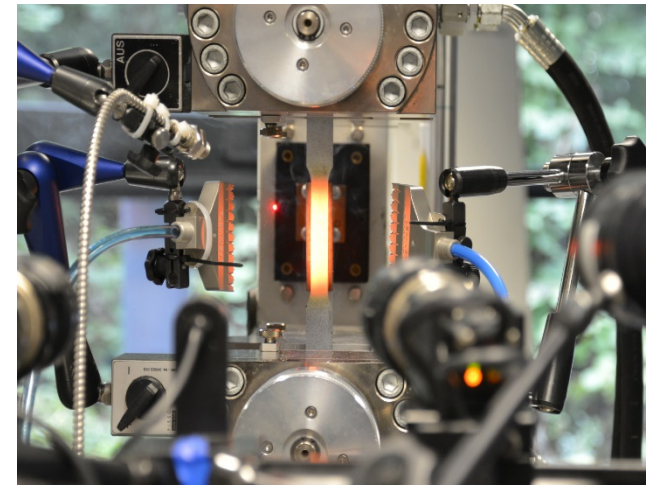
(* → drawing process not completed)

Electromagnetic Radius Calibration

- Increased forming limit
 - Decreased cup radius ($R_{DD} = 21\text{mm} \rightarrow R_{EM} = 13\text{mm}$)
 - Mainly caused by strain-rate change
 - No strain-path change required
 - No remaining quasi-static forming limit required
-

Electromagnetic Forming in the Flange

- Process analysis: Effect of coil position
- Process window: Discharge frequency f vs. Bulge height h
- Increased drawing ratio ($\beta_{\max} = 2.0 \rightarrow \beta_{\max,EM} = 2.1$)
- Increased forming depth (up to 73%)



Thank you for your attention.

This work is based on the results of PAK343.

We would like to thank the German Research Foundation (DFG) for its financial support.

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